

ORIGINAL RESEARCH PAPER

Study on Mass Transfer Enhancement in a Gas-Liquid System Using Nanomaterials

L. Saeednia^{1,2}, H. Hashemipour^{1,2,*}, D. Afzali²

¹Chemical engineering Department, University of Shahid Bahonar, Kerman, I.R. Iran

²International Center for Science, High Technology and Environmental Science, Mahan, Kerman, I.R.Iran

ARTICLE INFO.

Article history

Received 21 October 2013

Accepted 4 January 2015

Keywords

Gas Absorption

Gas Holdup

Mass Transfer Coefficient

Nanofluid

Nanostructure Materials

Abstract

The main objective of this paper is to examine the effect of nanomaterials on mass transfer coefficient in bubble type absorption of carbon dioxide by experiment. The absorption process is carried out in a bubble column and in room temperature. Mass transfer coefficient, saturated concentration of CO₂, and gas holdup are determined in this system. The kinds of nanomaterials, the concentrations of each one and the gas superficial velocity are considered as the key parameters. The results show that the mass fraction of nanomaterials has an optimum value to the mass transfer coefficient and saturated concentration of CO₂. 0.07% CNT nanofluid increases the mass transfer coefficient up to 78%. The superficial velocity of CO₂ enhances mass transfer coefficient and gas holdup within the experimental range, whilst it has no effect on saturated concentration of CO₂. In addition, nanomaterials in solution increase the gas holdup.

1. Introduction

In absorption processes, several techniques have been the key subject to enhance heat and mass transfer processes and obtain better performance of multiphase system within the recent years[1].

The techniques for the improvements are generally classified into mechanical treatment (such as heat transfer mode, the phases contact mode), the chemical treatment (such as additive adding) and the fluid properties improvement [2]. According to Kang et al. [3] experiment, the size of bubble absorber could be 47% smaller than that of falling film absorber in the

absorption performance of NH₃/H₂O. Adding of surface active agents into the liquid phase is a case of chemical treatment.

Surfactant changes the interfacial turbulence of the fluid that improves the heat and mass transfer coefficients.

Recently, nanofluids are known as one of the effective heat and mass transfer media[2]. Since the term “nanofluid” for enhancing heat transfer was firstly used by Choi [4], a large number of experimental studies have been performed on the investigating nanofluids with practical application to heat transfer[5].

A nanofluid is a suspension in which nanoparticles ($d_p < 100$ nm) are suspended uniformly in a base fluid[4].

Krishnamurthy et al. [6] first observed that a dye diffuses faster in a nanofluid than in water.

* Corresponding author

Email address: h-hashemipour@uk.ac.ir

Nomenclature			
C_A	Gas concentration in the liquid phase (g/L)	Q_g	Gas flow rate (L/min)
C_{As}	Saturated gas concentration in the liquid phase (g/L)	R_{eff}	Effective ratio of nanofluid (-)
H	Height of nanofluid in the absorber (Cm)	u	Gas superficial velocity (m/s)
H_0	Initial height of nanofluid in the absorber (Cm)	t	Dwell time (min)
$k_{L,a}$	Volumetric mass transfer coefficient (1/min)	ϵ_g	Gas hold up(-)

They explained that the Brownian motion of the nanoparticles induces convection in the nanofluids.

One of the most important applications of nanofluids in gas absorption is CO₂ removal from flue gases. CO₂ is one of the greenhouse gases which its control is becoming more important nowadays. Numerous studies have been carried out to enhance the CO₂ removal efficiency.

Astarita [7] used a Mono Ethanol Amine (MEA) solution to enhance the absorption performance by a reaction between the MEA and CO₂. Rao [8] perform the Hot Potassium Carbonate (HPC) process. Cullinane and Derks [9, 10] used a piperazine material to enhance the CO₂ absorption. Dagaonkar et al.[11] were the first researcher that reported the rate of gas absorption in a liquid phase may be enhanced considerably by the presence of particles in the liquid-phase. They added TiO₂microparticles to water to absorb CO₂.

In recent decade, nanofluid is known for its high thermal conductivity properties, and is can be used to enhance the heat and mass transfer processes of absorption.

In this research the effects of nanoparticles are investigated on the mass transfer enhancement in absorption of CO₂ in a bubble column system. Three types of nanostructural materials including CNT, TiO₂, and SiO₂ are used and the influences of mass fraction of nanomaterials and gas superficial velocity on mass transfer coefficient are studied.

2. Material and Method

2.1. Experimental study

Figure 1 shows the schematic diagram of the bubble absorption equipment.

The experimental setup consists of a cylindrical absorber test section with the diameter of 50 mm and length of 410 mm. Since the bubble-type absorber operates in the batch mode, the absorption process

operates in unsteady-state until it saturates. Volume of the nanofluid (as absorber) was fixed to 0.6 L at the room conditions during the experiments. The purity of CO₂ gas is 99.99 %.

The nanoparticles with a specific dosage are mixed and fully dispersed with the distilled water before the solution is charged into the nanofluid tank.

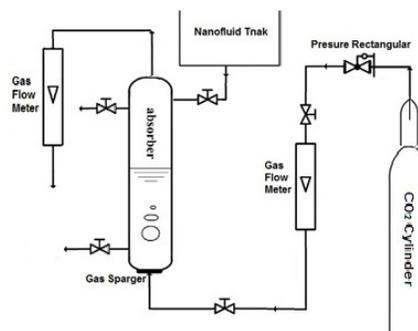


Fig. 1. Schematic diagram of the bubble absorption equipment

For the stable distribution of nanomaterials, the nanofluids are stirred for 20 hours and then be treated by the ultrasonic bath (Parasonic 2600) for 2 h. The nanofluid is filled up to a fixed volume in the nanofluid tank and then is discharged to the bubble absorber. Thereafter absorption begins when CO₂ enters the bubble absorber through a ceramic perforated plate sparger, which is located at the bottom of the absorber. The flow rate of CO₂ is measured by the gas flowmeter.

The gas flow rate is adjusted to allow the superficial gas velocity to be low enough in order to remaining in bubbly regime. The absorption rate is calculated by measuring the CO₂ concentration of the nanofluids using titration method. In this method, at first 5 mL of sample is mixed with 10-20 mL of sodium hydroxide, then a few drops of phenolphthalein are added to the solution as indicator, and hydrochloric acid is used as titrator to remove the

pink color of the solution. In the next step, a few drops of methyl orange are added to the solution and titration is continued until the orange color of the solution is changed to yellow.

This point is the equivalent and the used amount of hydrochloric acid indicates the concentration of CO₂ in the solution. In case of CNT nanofluids, due to the black color of the solution the equivalent point is determined by the changes in pH of the solution. All experimental data are repeatable with a negligible error.

In the experiments three kind of nanostructure material are used to prepare nanofluids. The properties of the nanomaterials are summarized in table 1.

In this study, different mass fractions of nanomaterials are experimented. The nanofluid containing TiO₂ and SiO₂ nanoparticles are prepared with 0.01, 0.05, 0.1 and 0.5 Wt. %, while CNTs are added with 0.01, 0.05, 0.07 and 0.1 Wt. %.

Table 1
Properties of nanomaterials.

Nano material	Producer	Average Size (nm)	Surface area (m ² /g)
CNT	RIFI	D=10-30, L=100	105
TiO ₂	Degussa	21	50
SiO ₂	Degussa	12	200

2.2. Modeling study

The mass balance on liquid phase of the bubble column leads to the ordinary differential equation 1 assuming perfect mixing, mass transfer between two phases without reaction in the unsteady state.

$$\frac{dc_A}{dt} = k_L a (c_{As} - c_A) \quad (1)$$

Where C_A is CO₂ concentration in the liquid phase, C_{AS} is the saturated concentration of CO₂ in the liquid phase and k_{LA} is the volumetric mass transfer coefficient. Solving the equation 1 results equation 2 to obtain the mass transfer coefficient

$$c_A = c_{As} \left(1 - \frac{1}{e^{k_L a t}}\right) \quad (2)$$

The volumetric mass transfer coefficient (k_{LA}) is determined by plotting the experimental C_A values versus time, while C_{AS} has a fixed amount for any

nanofluid. Differentiation of equation 2 results to the rate of absorption as a function of time as equation 3.

$$\frac{dc_A}{dt} = k_L a C_{As} e^{-k_L a t} \quad (3)$$

In order to analyze the effect of nanofluid on the mass transfer rate, the effective ratio (R_{eff}) is defined as equation 4.

$$R_{eff} = \frac{(k_L a)_{nanofluid}}{(k_L a)_{water}} \quad (4)$$

The physical meaning of the effective ratio is ‘the effectiveness of the nanofluid for mass transfer coefficient enhancement. Amount of this parameter shows how much the nanoparticles improve the mass transfer coefficient.

For the bubble column experiments, the gas holdup that varies with gas velocity and nanoparticle concentrations is measured using the liquid expansion method, which is indicated in the equation 5.

In this method, the initial liquid height in the column and the height after gassing the column are measured. The gas hold up is calculated by using following equation:

$$\epsilon_g = \frac{H - H_0}{H} \quad (5)$$

In this equation H₀ is the initial height of nanofluid and H is the height of nanofluid after entering CO₂ into the column.

3. Results and Discussion

3.1. Effect of mass fraction of nanomaterials on absorption amount

Figures (2-4) display the experimental data of CO₂ concentration in the liquid phase during the time in different dosage of CNT.

As it is observed the absorption amount increases with increasing of the nanoparticles mass fraction sharply at first, then gradually fix. From figure 2 it can be understood that the 0.07% CNT nanofluid has the maximum absorption amount.

Figures 3 and 4 demonstrate that in TiO₂ nanofluids, the maximum amount of CO₂ is absorbed when 0.05% of TiO₂ and 0.1% of SiO₂ nanoparticles are added to distilled water.

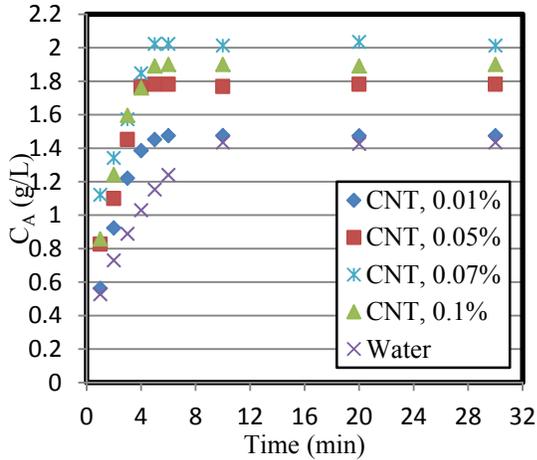


Fig. 2. Variation of CO₂ concentration in liquid phase with time in different CNT dosage ($Q_g=0.5$ L/min)

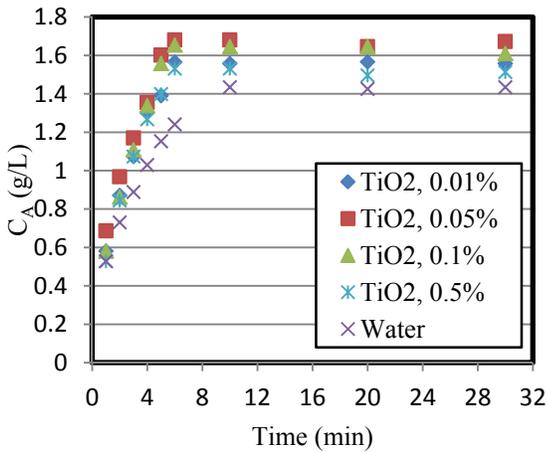


Fig. 3. Variation of CO₂ concentration in liquid phase with time in different TiO₂ nanoparticle dosage ($Q_g=0.5$ L/min)

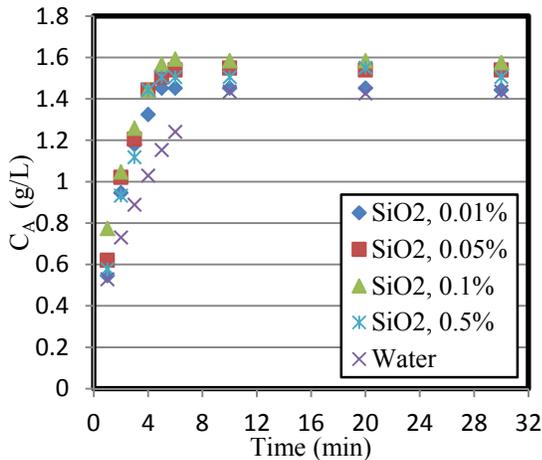


Fig. 4. Variation of CO₂ concentration in liquid phase with time in different SiO₂ nanoparticle dosage ($Q_g=0.5$ L/min)

The nanoparticles can be agglomerate at high dosage and in this condition increasing in the nanoparticle dosage do not improve the CO₂ removal. This can be reason of selection of no higher dosage as the optimum dosage in the Co₂ removal.

In addition, the absorption amount of carbon dioxide in liquid phase increases to an approximate constant amount, which is the saturation concentration of CO₂. The use of nanomaterials increases the saturation of CO₂. The values of CO₂ saturated concentration in nanofluids with optimum mass fraction of nanomaterials are illustrated in table 2.

It can be concluded that 0.07% CNT nanofluid absorbs the maximum amount of CO₂. This nanofluid enhances the saturated concentration of CO₂ up to 40%.

3.2. Effect of mass fraction of nanomaterials on volumetric mass transfer coefficient

The volumetric mass transfer coefficient ($k_L a$) is calculated for water and each nanofluid using curve fitting of experimental data presented in figures (2-4) in equation 2. All R² values of curve fittings are more than 98%, therefore the selected model is seemed to be accurate.

These correlations give term ($k_L a$) for CO₂ removal using nanofluids. Then the effective ratio is determined from equation 4. Figure 5 expresses the effective ratio with respect to the mass fraction of CNT, TiO₂ and SiO₂ nanoparticles.

Table 2
Gas phase reactions [21].

nanomaterial	CNT	SiO ₂	TiO ₂
Optimum Mass fraction (%)	0.07	0.05	0.1
CAs (g/L)	2.046	1.697	1.597

Since the effective ratios of all nanofluids are higher than 1.0, it is undoubtedly implied that nanofluids can enhance the mass transfer coefficient, so improve the absorption performance.

It also can be inferred that the effective ratio increases with the mass fraction of nanofluids increasing at first, then decreases. The maximum effective ratio is 1.78 in the case of nanofluid with 0.07% carbon nanotubes.

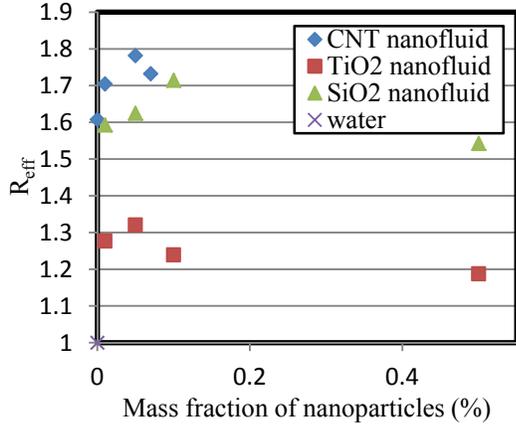


Fig. 5. Effective ratio in different nanoparticles dosage in the liquid phase ($Q_g=0.5$ L/min)

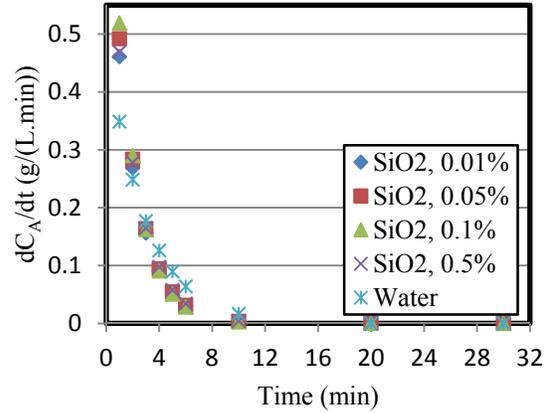


Fig. 8. Absorption rate in different concentrations of SiO_2 nanofluid ($Q_g=0.5$ L/min)

3.3. Effect of mass fraction of nanomaterials on absorption rate

The rate of absorption (dC_A/dt) is determined based on equation 3 using calculated data $K_L a$, and C_{As} .

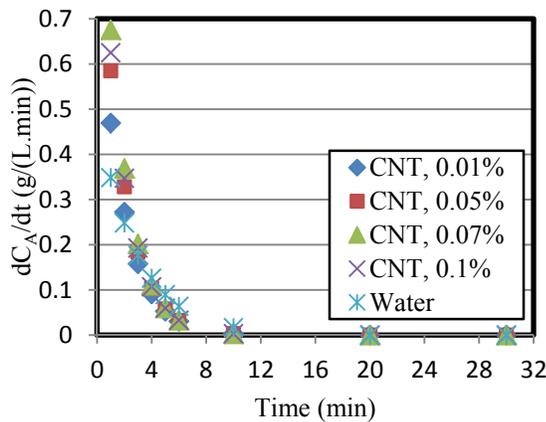


Fig. 6. Absorption rate in different concentrations of CNT nanofluid ($Q_g=0.5$ L/min)

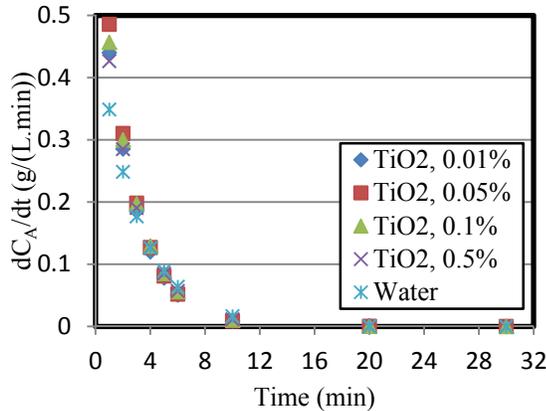


Fig. 7. Absorption rate in different concentrations of TiO_2 nanofluid ($Q_g=0.5$ L/min)

Figures 6 to 8 show the absorption rate versus time in water and nanofluids.

As it is observed in these figures the absorption rate was decreased by the time due to the absorber of a batch system. The absorption rate increases with the mass fraction of nanomaterials increasing at first, then it gradually fix. The mechanisms of the nanofluid enhancing bubble absorption have four possible factors as follows.

Nanomaterials in the nanofluids can cause the micro-convection in liquid phase because of the Brownian motion of nanomaterials. This micro-convection can improve the mass diffusion of CO_2 gas in the nanofluid. According to the Krishnamurthy's experiment [6], the enhancement of the diffusion coefficient firstly increases with the mass fraction of the nanoparticles increasing, and then decreases. Nanomaterials in the nanofluid can cause the grazing effect, which was described by Kars et al. [12] and Alper et al. [13].

The grazing effect is that the particles in the liquid adsorb gas molecules in the gas-liquid interface, then move right through the concentration boundary layer, finally pick up the adsorbate in the bulk liquid. According to Reference [12], the enhancement of the grazing effect on absorption firstly increases with increasing the mass fraction of particles, and then remains constant.

The effects of the concentration of nanomaterials on the enhancement of mass diffusion and grazing effect can explain just the deviating trend of the absorption rate with the mass fraction of nanomaterials. Fan et al. [14] found that the gas holdup in the nanofluid is higher than that of water at the same flow rate of the gas.

The increase in the gas holdup can lead to an increase in the area of the gas–liquid interface for the same flow rate of CO₂ gas. Therefore improve the absorption rate of the CO₂. Nanoparticles in the nanofluid can increase the thermal conductivity of liquid phase and the heat transfer in the absorption process. Absorption process is a combined heat and mass transfer process. The improvement of heat transfer can decrease the temperature at the gas–liquid interface; increase the absorption potential of liquid phase. So enhance the absorption rate of the CO₂.

3.4. Effect of type of nanomaterials on gas holdup

The gas holdup is a main factor in characterization of the bubble column operation. Table 3 demonstrates the gas holdup values obtained by using equation 5, in different nanofluids.

Table 3
Gas holdup in mass fraction 0.1% nanomaterial.

Liquid Phase	Distilled water	CNT	TiO ₂	SiO ₂
εg	00.015	0.017	0.018	0.020

The results indicate that the gas holdup in the nanofluid is consistently higher than that in water. According to Fan et al.[14] the difference in the gas holdup between the nanofluid and water in the bubble column experiment can be related to the differences in bubble size. They found that the bubble size in nanofluids is smaller than in water, and the smaller bubbles results in larger gas holdup. In our experiment 0.1% of SiO₂ nanoparticles in water caused the maximum gas holdup.

3.5. Effect of superficial gas velocity on absorption amount

Figures (9-11) reveal the absorption amount of CO₂ in nanofluid for the different superficial gas velocities. The flow rates of CO₂ are adjusted to 0.5, 1 and 1.5 L/min, which results to superficial gas velocities of 0.004, 0.008 and 0.012 m/s, respectively, and the mass fraction of nanomaterials in the nanofluids is 0.05%.

The experimental data show that slope of the curve which is the absorption rate is increased with

increasing superficial gas velocities for each nanomaterial.

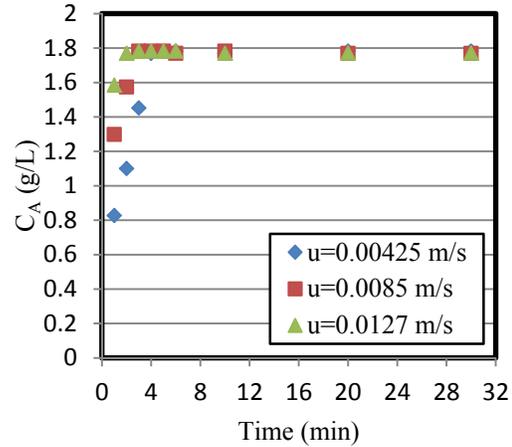


Fig. 9. CO₂ concentration in 0.05% CNT nanofluid in different superficial gas velocities

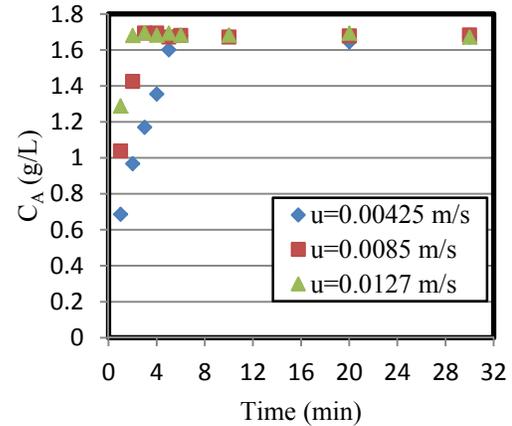


Fig. 10. CO₂ concentration in 0.05% TiO₂ nanofluid in different superficial gas velocities

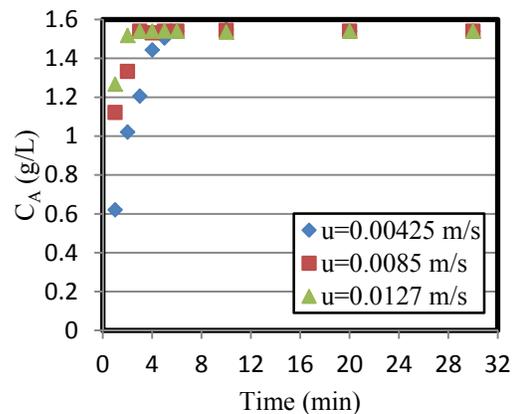


Fig. 11. CO₂ concentration in 0.05% SiO₂ nanofluid in different superficial gas velocities

This indicates that mass transfer rate and time of saturation are affected by the superficial gas velocity of the gas, although the saturated concentration of CO_2 does not change with the velocity.

3.6. Effect of superficial gas velocity on volumetric mass transfer coefficient

The superficial gas velocity as another main factor affecting in the column operation is calculated as dividing the inlet gas volumetric flow rate to the column section area. Figure 12 shows the mass transfer coefficient in water and optimum concentration of nanofluids in different superficial velocities of CO_2 .

The mass transfer coefficient increases almost linearly with increasing the superficial gas velocity. The superficial gas velocity affects the grazing effect because of variation of the disturbance of the nanofluid [1]. Thus the increase of superficial velocity of CO_2 improves remarkably the grazing effect of the nanofluids.

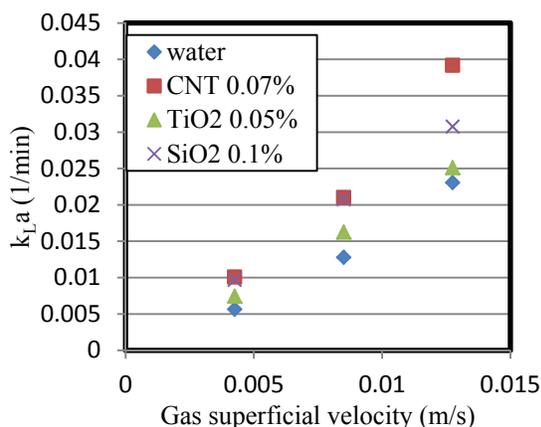


Fig. 12. Mass transfer coefficient in different superficial gas velocities

3.7. Effect of superficial gas velocity on gas holdup

The present experimental study reveals the superior gas hold up in nanofluids. It is also observed that the gas holdup in a bubble column increases significantly when superficial gas velocity increases. This behavior is remarkable for nanomaterials related to water and SiO_2 in comparison with the other nanomaterials. These results are demonstrated in figure 13.

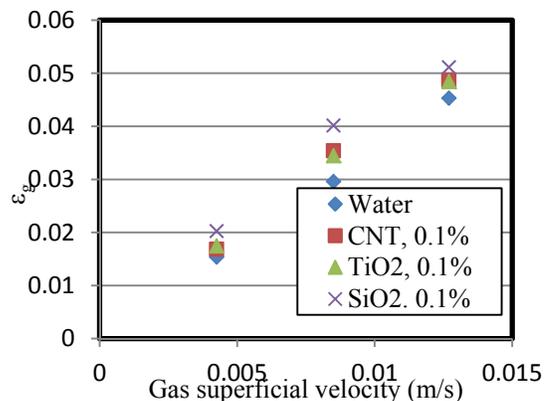


Fig. 13. Gas holdup in different superficial velocities in nanofluids and water

4. Conclusion

In this study, the CO_2 gas absorption using different nanofluids in a bubble column was investigated experimentally. The kinds of nanoparticles and the concentrations of each nanoparticle and the superficial velocity of CO_2 are considered as the key parameters.

It can be concluded that addition of nanomaterials enhances the mass transfer coefficient and saturation concentration of CO_2 in liquid phase and therefore the absorption performance during the bubble absorption process. The maximum effective ratio is 1.78 when 0.07% of carbon nanotubes are added to water. CNT is the most effective nanomaterials among the considered nanomaterials. The mass fraction of nanomaterials has an optimum value to the effective ratio of the nanofluids.

The results also showed that the superficial velocity of CO_2 enhances mass transfer coefficient within the experimental range.

Gas holdup in nanofluids is higher than water, and increases with increasing nanomaterials concentration and gas superficial velocity. The enhancement mechanism by nanoparticles for absorption performance can be explained by the grazing effect, but the distinct mechanism is not developed yet. The additional analytical study should be carried out to clarify the enhancement mechanism of mass transfer performance.

References

- [1] R. Bacon, Growth, Structure, and Properties of Graphite Whiskers, *Appl. Phys. Lett* 31(2) (1960) 283-290.

- [2] J.K.Kim, J.Y.Jung., Y. T.Kang., The effect of nano-particles on the bubble absorption performance in a binary nanofluid. *International Journal of Refrigeration* 29 (2006) 22–29.
- [3] Y.T.Kang, A. Akisawa, T. Kashiwagi., Analytical investigation of two different absorption modes: falling film and bubble types. *International Journal of Refrigeration* 23 (2000) 430–443.
- [4] S.U.S.Choi, Enhancing thermal conductivity of fluids with nanoparticles. ASME International Mechanical Engineering Congress and Exposition, San Francisco, California November (1995)12-17.
- [5] Wun-gwi Kim, Hyun Uk Kang, Kang-min Jung, Sung Hyun Kim., Synthesis of Silica Nanofluid and Application to CO₂ Absorption. *Separation Science and Technology* 43 (2008) 3036–3055.
- [6] S.Krishnamurthy, P. Bhattacharya, P.E. Phelan, Enhanced Mass Transport in Nanofluids, *Nano Letters* 6 (2006) 419–423.
- [7] G.Astarita, Carbon dioxide absorption in aqueous monoethanolamine Solutions. *Chemical Engineering Science* 16 (1961) 202–207.
- [8] D.P.Rao, Design of a packed column for absorption of carbon dioxide in DEA promoted hot K₂CO₃ solution. *Gas Separation and Purification* 4 (1990) 58–61.
- [9] J.T.Cullinane, G.T.Rochelle, Carbon dioxide absorption with aqueous potassium carbonate promoted by piperazine. *Chemical Engineering Science* 59 (2004) 3619–3630.
- [10] P.W.J Derks, T. Kleingeld, C.V. Aken, J.A. Hogendoorn, G.F.Versteeg, Kinetics of absorption of carbon dioxide in aqueous piperazine solutions. *Chemical Engineering Science* 61(2006) 6837–6854.
- [11] M.V.Dagaonkar, H.J. Heeres, A.A.C.M. Beenackers, V.G. Pangarkar., The application of fine TiO₂ particles for enhanced gas absorption. *Chemical Engineering Journal* 92 (2003)151–159.
- [12] R.L.Kars, R.J.Best, A.A.H.Drinkenburg, The sorption of propane in slurries of active carbon in water. *Chemical Engineering Journal* 17 (1979) 201–210.
- [13] Alper, E., Wichtendahl, B., Deckwer, W.D., Gas Absorption mechanism in catalytic slurry reactors. *Chemical Engineering Science* 35 (1980) 217–222.
- [14] L.S. Fan, O. Hemminger, Z.Yu, F. Wang, Bubbles in nanofluids. *Industrial and Engineering Chemistry Research* 46 (2007) 4341–4346.